## Notes on the GSW code gsw\_z\_from\_p for calculating height *z* from pressure *p*

Height z is measured positive upwards, so it is negative in the ocean. First, note that we use the following version of specific volume anomaly,

$$\delta = \hat{v}(S_A, \Theta, p) - \hat{v}(S_{SO}, 0^{\circ}C, p). \tag{1}$$

That is, the reference Absolute Salinity is the Absolute Salinity of the Standard Ocean,  $S_{SO} = 35.165~04~{\rm g~kg^{-1}}$ , and the reference "temperature" is a fixed value of Conservative Temperature of zero degrees Celsius. Dynamic height anomaly  $\Psi$  is then defined by Eqn. (3.27.1) of IOC *et al.* (2010) as follows

$$\Psi = -\int_{P_0}^{P} \delta(p') dP', \qquad (2)$$

where  $P_0 = 101 325 \,\mathrm{Pa}$  is the standard atmosphere pressure.

The vertical integral of the hydrostatic equation  $(P_z = -g \rho \text{ or } g = -v P_z)$  is

$$\int_{0}^{z} g(z') dz = -\int_{P_{0}}^{P} v(p') dP' = -\int_{P_{0}}^{P} \hat{v}(S_{SO}, 0^{\circ}C, p') dP' + \Psi$$

$$= -\hat{h}(S_{SO}, 0^{\circ}C, p) + \Psi.$$
(3)

We use the 48-term based expression (Eqn. A.30.6) for enthalpy, recognizing that because  $\Theta = 0^{\circ}\text{C}$  many of the coefficients on pages 121-123 of the TEOS-10 Manual are zero, so the evaluation of Eqn. (A.30.6) is less computationally expensive than it may appear. Let us write the gravitational acceleration of Eqn. (D.3) of IOC *et al.* (2010) as

$$g = g(\phi, z) = g(\phi, 0)(1 - \gamma z),$$
 (4)

so that Eqn. (3) becomes

$$\hat{h}^{48}(S_{SO}, 0^{\circ}C, p) - \Psi + g(\phi, 0)(z - \frac{1}{2}\gamma z^{2}) = 0.$$
 (5)

When the  $\mathbf{gsw_z}$ -from\_p code is called with two arguments, as in  $\mathbf{gsw_z}$ -from\_p(p,lat), we ignore  $\Psi$  and solve this quadratic expression for the height z from Eqn. (5) (using the standard quadratic solution equation, but for  $z^{-1}$ .) Note again that height z is negative in the ocean. When the code is called with three arguments, the third argument is taken to be the dynamic height anomaly  $\Psi$  and this is used in the solution of Eqn. (5). Dynamic height anomaly can be evaluated using the GSW function  $\mathbf{gsw_geo_strf_dyn_height_CT}$ .

## Notes on the GSW code gsw\_p\_from\_z for calculating pressure p from height z

In the  $\mathbf{gsw_p\_from_z}$  code we evaluate pressure p using a modified Newton-Raphson iteration procedure so that the pressure so obtained is exactly consistent with the "forward" calculation of z from p via the function  $\mathbf{gsw_z\_from_p}$ .

When the  $gsw_p_from_z$  code is called with two arguments, as in  $gsw_p_from_z(z,lat)$ , we ignore  $\Psi$  while solving Eqn. (6) below. Note again that height z is negative in the ocean. When the code is called with three arguments, the third argument is taken to be the dynamic height anomaly  $\Psi$  and this is used in the solution of Eqn. (6).

A good starting point is the Saunders (1981) quadratic (note that the Saunders paper and the corresponding SeaWater code are for depth not height). So, given z we have a zeroth estimate of pressure,  $p_0$ , from the Saunders (1981) quadratic expression. Now we want to solve

$$f(p) = 0$$
, where  $f(p) = \hat{h}^{48}(S_{SO}, 0^{\circ}C, p) - \Psi + g(\phi, 0)(z - \frac{1}{2}\gamma z^{2})$ . (6)

The derivative of f(p) is approximately

$$f'(p) = 10^4 \hat{v}^{48} (S_{SO}, 0^{\circ}C, p),$$
 (7)

and this is available from the 48-term rational function expression for seawater density (and since  $\Theta=0^{\circ}\mathrm{C}$ ,  $\hat{v}^{48}\left(S_{\mathrm{SO}},0^{\circ}\mathrm{C},p\right)$  is particularly simple to evaluate). The factor of  $10^4$  in Eqn. (7) is because we want to solve for pressure in dbar rather than in the natural SI unit for pressure of Pa . That is, Eqn. (7) is the derivative of  $f\left(p\right)$  with respect to pressure p in dbar.

After finding  $p_0$  we evaluate  $f\left(p_0\right) = \hat{h}^{48}\left(S_{\text{SO}}, 0^{\circ}\text{C}, p_0\right) - \Psi + g\left(\phi, 0\right)\left(z - \frac{1}{2}\gamma\,z^2\right)$ , then calculate  $f'\left(p_0\right) = 10^4\,\hat{v}^{48}\left(S_{\text{SO}}, 0^{\circ}\text{C}, p_0\right)$  and use these values of  $f\left(p_0\right)$  and  $f'\left(p_0\right)$  to form an intermediate pressure estimate  $p_1$  as

$$p_1 = p_0 - f(p_0)/f'(p_0)$$
 (8)

Then we form  $p_{\rm m}=0.5\big(p_0+p_1\big)$  and evaluate  $f'\big(p_{\rm m}\big)=10^4\,\hat{v}^{48}\big(S_{\rm SO},0^{\circ}{\rm C},p_{\rm m}\big)$  and use  $f\big(p_0\big)$  and  $f'\big(p_{\rm m}\big)$  to get  $p_2$  from

$$p_2 = p_0 - f(p_0)/f'(p_m)$$
 (9)

This is one full step of the "modified Newton-Raphson" iteration procedure and this one modified step gives pressure to better than  $1.6x10^{-10}$  dbar (which is essentially machine precision) down to a height z of -8000m. The  $\mathbf{gsw_p\_from_z}$  function performs this one full iteration of the modified Newton-Raphson iteration.