



BOUSSOLE DATA PROCESSING

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21-23 February 2017 – FRM4SOC

OUTLINE

- > Preprocessing
 - conversion to physical units
 - dark subtraction
 - data reduction
- > Processing
 - conversion to physical units
 - depth correction
 - cosine correction
 - shading correction
 - extrapolation
 - *Rrs*
- > Quality Control
 - biofouling
 - intercalibration

APPLICATION OF FACTORY CALIBRATION

> Satlantic, NIST traceable, every 6-12 months

$$\begin{aligned}
 - E_s(t', \lambda)_{Dd} &= [E_s(t', \lambda)_{Volt} - Dark_{Cal_{Es}}(\lambda)] \cdot Lin_{Cal_{Es}}(\lambda) \\
 - L_u(z', t', \lambda)_{Dd} &= [L_u(z', t', \lambda)_{Volt} - Dark_{Cal_{Lu(z)}}(\lambda)] \cdot Lin_{Cal_{Lu(z)}}(\lambda) \cdot Imm_{Cal_{Lu(z)}}(\lambda) \\
 - E_d(z', t', \lambda)_{Dd} &= [E_d(z', t', \lambda)_{Volt} - Dark_{Cal_{Ed(z)}}(\lambda)] \cdot Lin_{Cal_{Ed(z)}}(\lambda) \cdot Imm_{Cal_{Ed(z)}}(\lambda) \\
 - E_u(z', t', \lambda)_{Dd} &= [E_u(z', t', \lambda)_{Volt} - Dark_{Cal_{Eu(z)}}(\lambda)] \cdot Lin_{Cal_{Eu(z)}}(\lambda) \cdot Imm_{Cal_{Eu(z)}}(\lambda)
 \end{aligned}$$

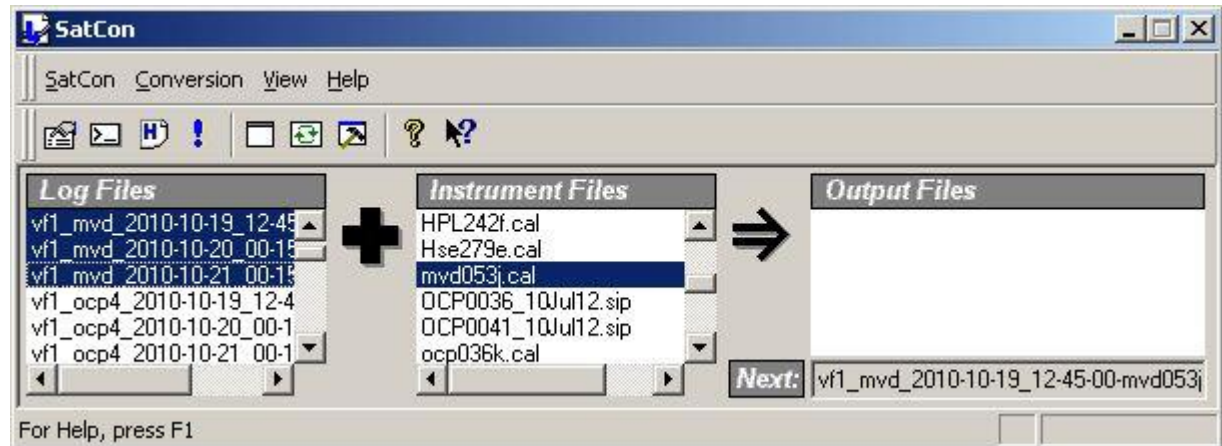
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#
# MVDS s/n 053 with OCI-200 s/n 095
#
# Final calibration file valid 13 November, 2014
# Villefranche / Project 2007-503

INSTRUMENT SATMVD '' 6 AS 0 NONE
SN 0053 '' 4 AI 0 NONE
RATE 6 'Hz' 0 BU 0 NONE

# Optical data updated by Jennifer

#ES sensor OCI-200 S/N 095 calibrated for LO GAIN in IN AIR
# by Jenn on 11/13/14 at 10:38:11
# LO GAIN calibration, LAMP: f1304 at DIST: 50.0 cm
ES 412.3 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32774.3 9.72971e-003 1.00
ES 442.3 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32775.2 9.45316e-003 1.00
ES 489.5 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32775.6 9.08008e-003 1.00
ES 510.6 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32775.9 9.79014e-003 1.00
ES 560.2 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32775.1 9.09505e-003 1.00
ES 669.5 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32776.7 8.61297e-003 1.00
ES 682.3 'uW/cm^2/nm' 2 BU 1 OPTIC2
  32773.0 9.35531e-003 1.00
    
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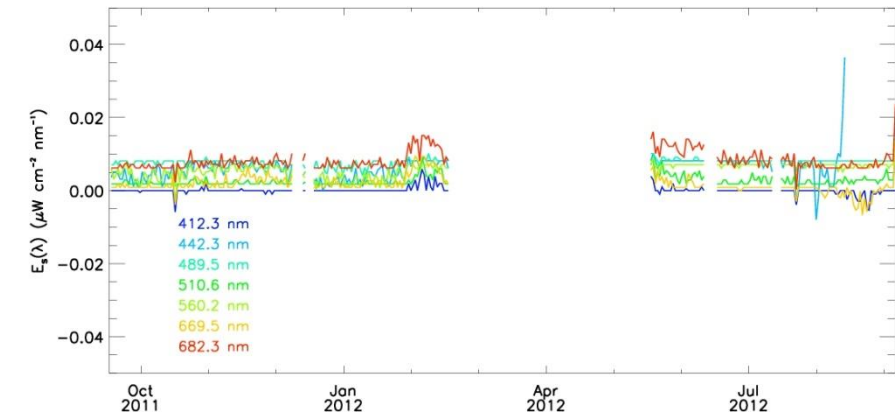
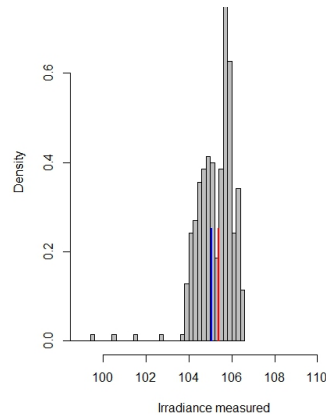
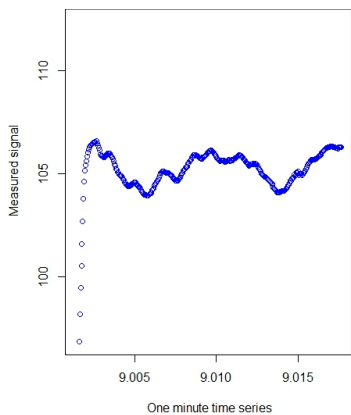
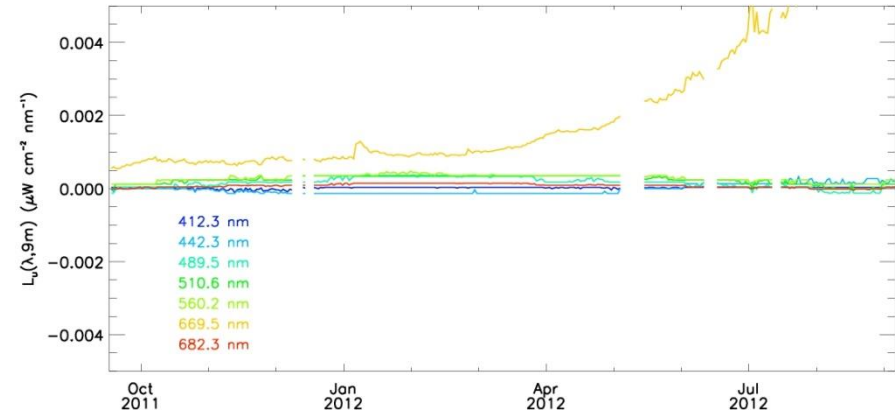
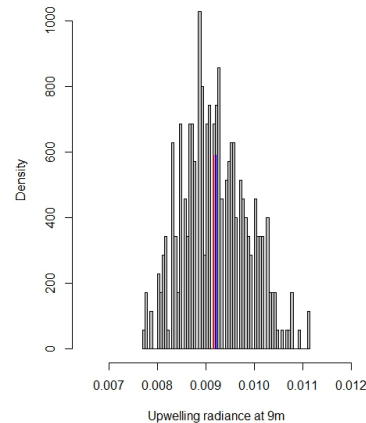
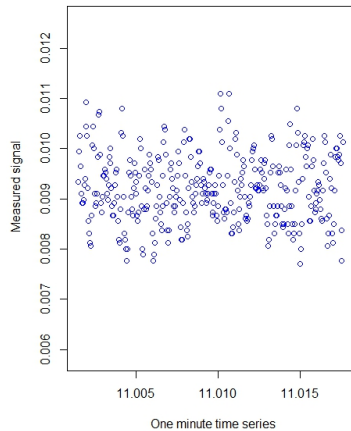
MULTISPECTRAL INSTRUMENTS (NO INTERNAL SHUTTER)

> The median value of 1' records is retained as representative of each quarter (same for ancillary)

- $\overline{E_s(t, \lambda)_{Dd}} = \text{median}[E_s(t', \lambda)_{Dd}]_{t'=0s}^{60s}$
- $\overline{L_u(z, t, \lambda)_{Dd}} = \text{median}[L_u(z', t', \lambda)_{Dd}]_{t'=0s}^{60s}$

> An average daily dark is calculated from night binned measurements and subtracted

- $\overline{E_s(t, \lambda)'} = \overline{E_s(t, \lambda)_{Dd}} - \text{mean}[E_s(t, \lambda)_{Dd}]_{t=22h}^{3h}$
- $\overline{L_u(z, t, \lambda)'} = \overline{L_u(z, t, \lambda)_{Dd}} - \text{mean}[L_u(z, t, \lambda)_{Dd}]_{t=22h}^{3h}$



Mean and median not significantly different when the measurement is not affected by environmental variability (e.g. clouds)

HYPERSPECTRAL INSTRUMENTS (INTERNAL SHUTTER)

> The mean of two consecutive dark measurements is subtracted to light measurements in between

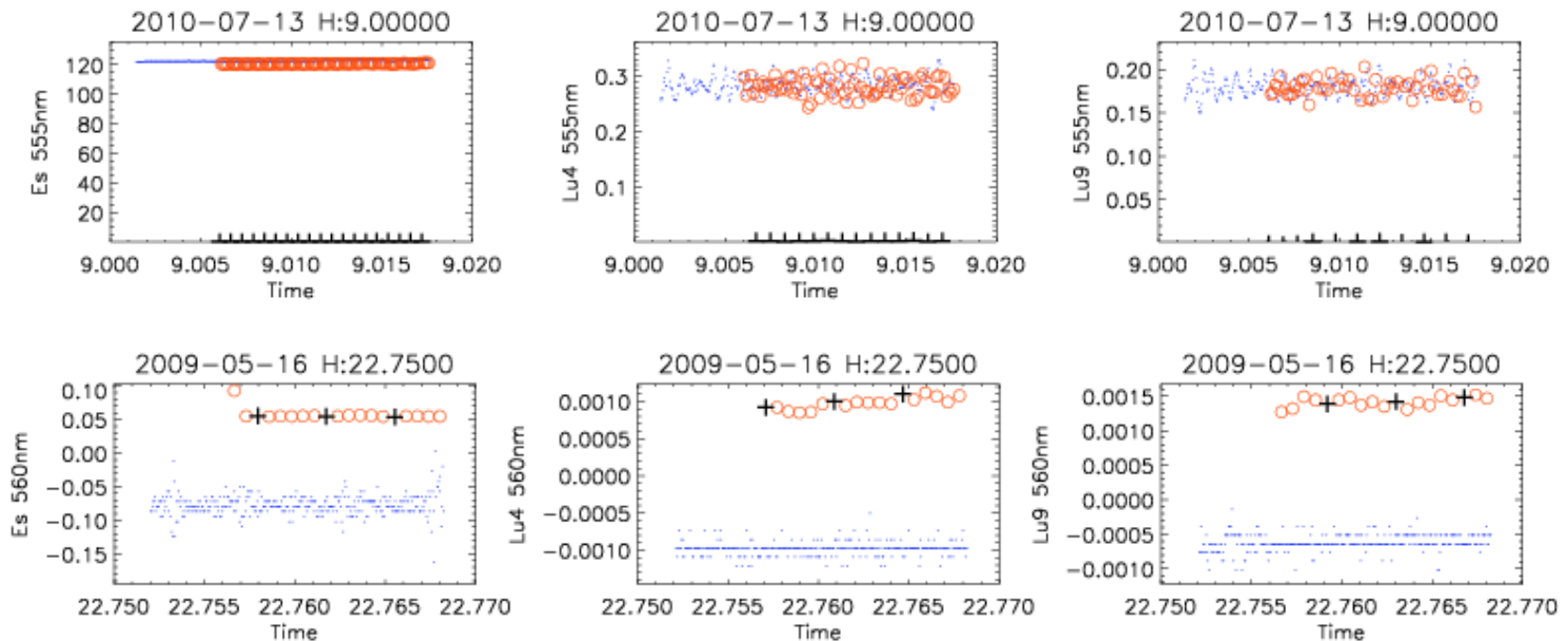
$$- E_s(t', \lambda) = E_s(t', \lambda)_{Dd} - \frac{E_s(t'-1, \lambda)_{Shutter} + E_s(t'+1, \lambda)_{Shutter}}{2}$$

$$- L_u(z', t', \lambda) = L_u(z', t', \lambda)_{Dd} - \frac{L_u(z', t'-1, \lambda)_{Shutter} + L_u(z', t'+1, \lambda)_{Shutter}}{2}$$

> Then the median value is kept for each quarter

$$- \overline{E_s(t, \lambda)}' = \text{median}[E_s(t', \lambda)]_{t=0}^{60s}$$

$$- \overline{L_u(z, t, \lambda)}' = \text{median}[L_u(z', t', \lambda)]_{t=0}^{60s}$$

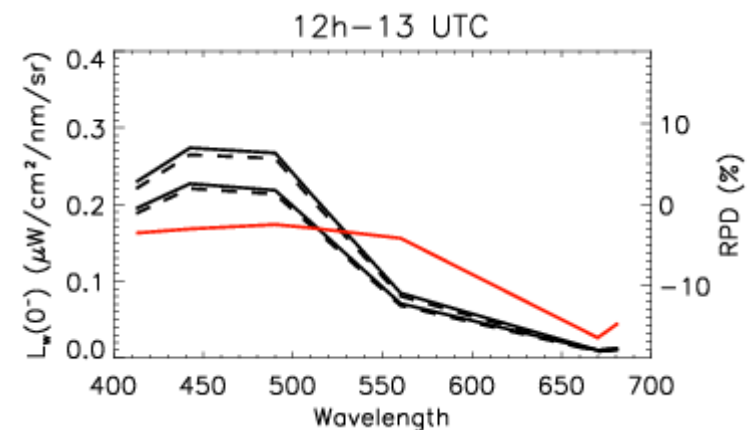
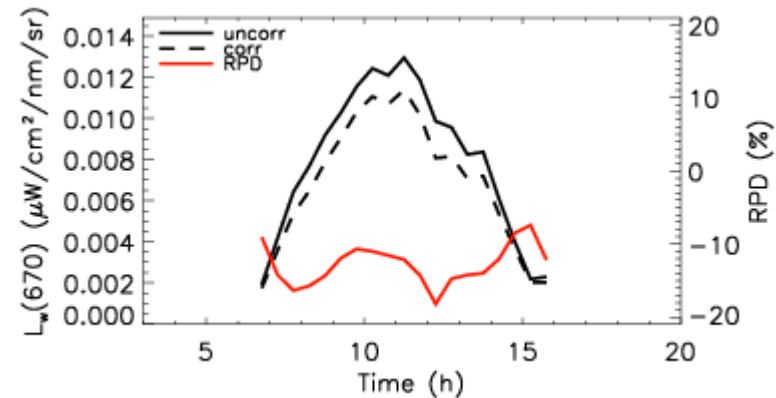
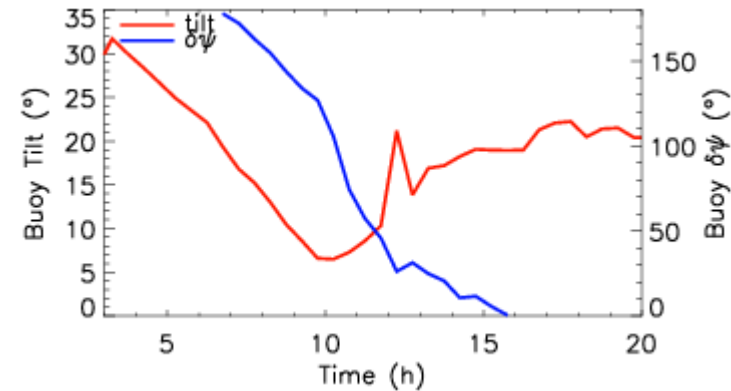
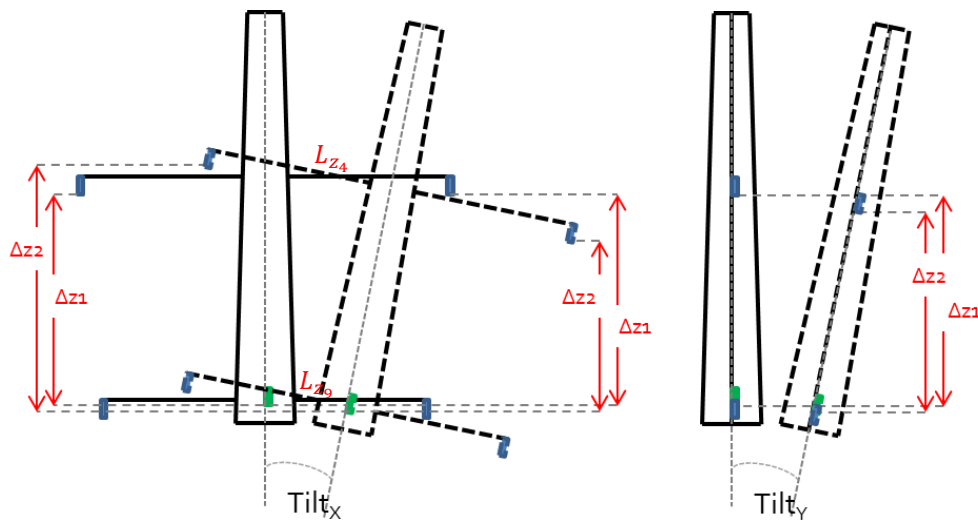


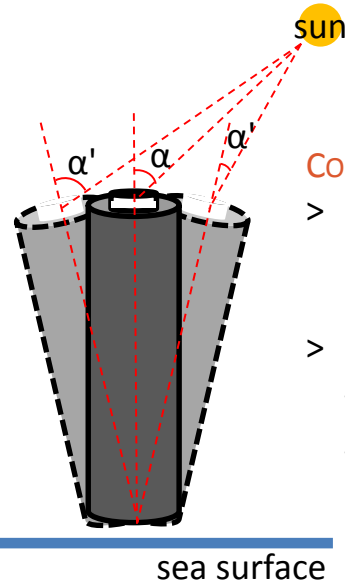
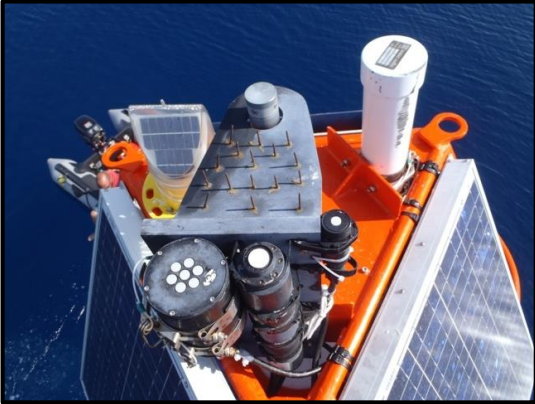
CORRECTION OF INSTRUMENT DEPTH

- > Depth, $Tilt_x$ and $Tilt_y$ are measured in the core of the buoy
- > The distance of each radiometer from the CTD along the buoy principal axis is known, so its depth when $Tilt=0$
- > A correction factor for depth each instrument and measurement is derived from the buoy Tilt and applied

$$z_{rad}(t) = [z_{CTD}(t) - \Delta z_{rad}] \cdot f_{depth}(t, Tilt_x, Tilt_y)$$

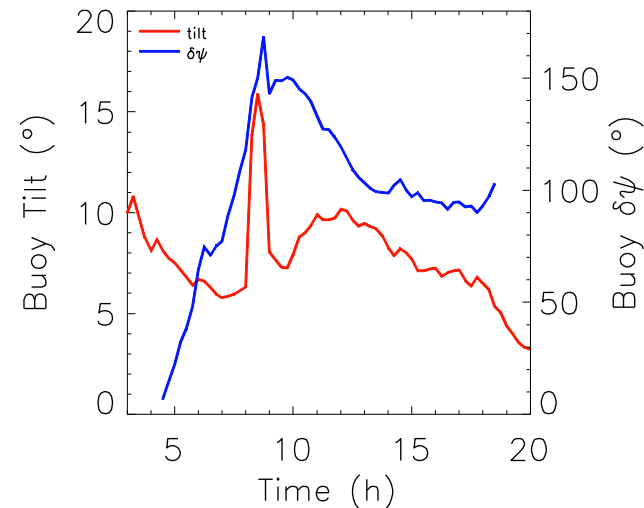
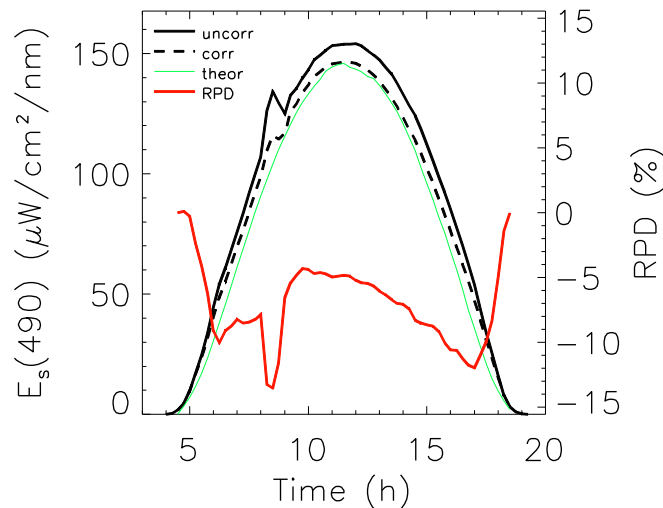
$$f_{depth}(t) = (1 - \cos Tilt_y(t)) \cdot (1 - \cos Tilt_x(t)) - L_{z_{rad}} \sin Tilt_x(t)$$

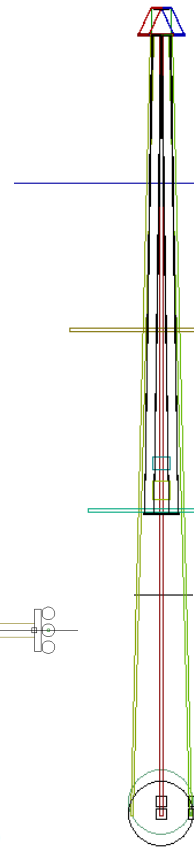




COSINE CORRECTION OF SURFACE IRRADIANCE

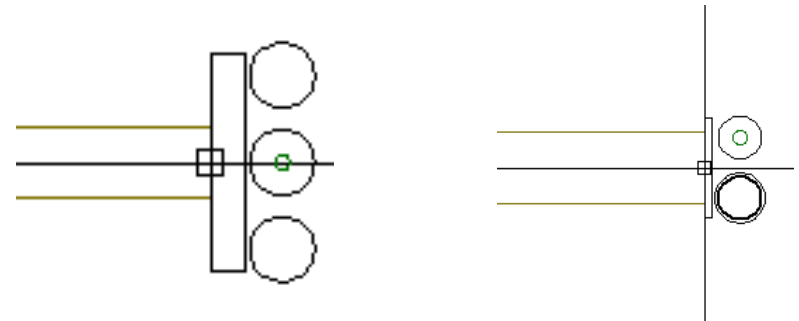
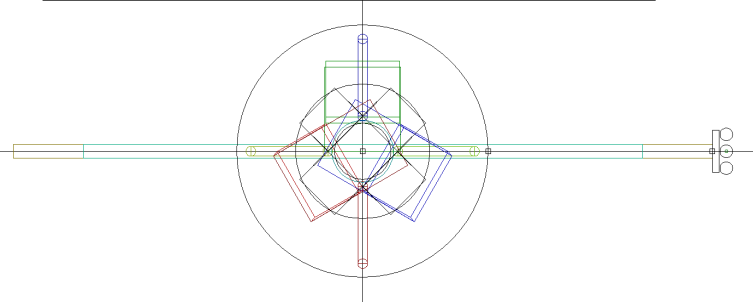
- > First the direct fraction of E_s is estimated following *Gregg & Carder, 1990*
 - $\overline{E_s(t, \lambda)'} = \overline{E_s(t, \lambda)'} \cdot f_{dir} + \overline{E_s(t, \lambda)'} \cdot (1 - f_{dir})$
- > The correction is then applied to the direct fraction of E_s
 - $E_s(t, \lambda) = \overline{E_s(t, \lambda)'} \cdot f_{dir} \cdot f_{tilt} + \overline{E_s(t, \lambda)'} \cdot (1 - f_{dir})$
 - Where $f_{tilt} = \frac{\cos(\alpha')}{\cos(\alpha)}$





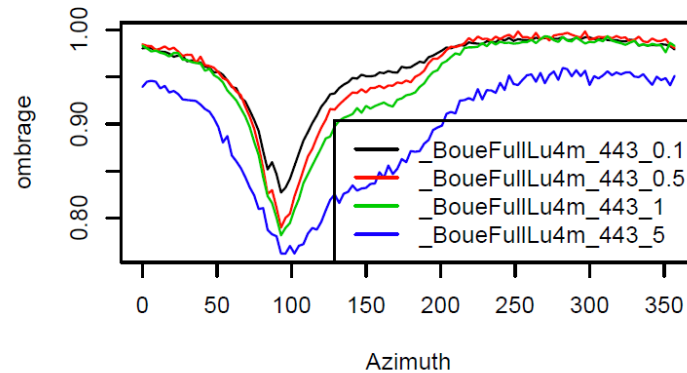
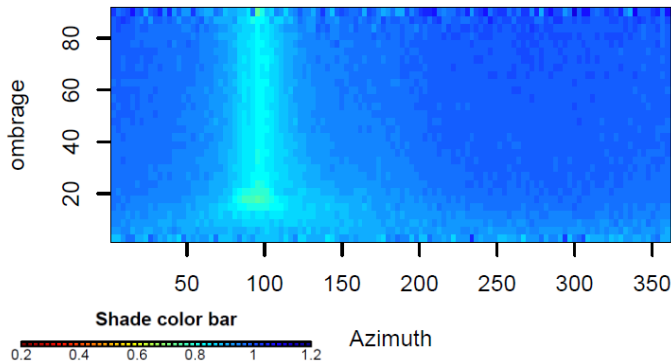
BUOY STRUCTURE SHADING AND INSTRUMENT SELF-SHADING

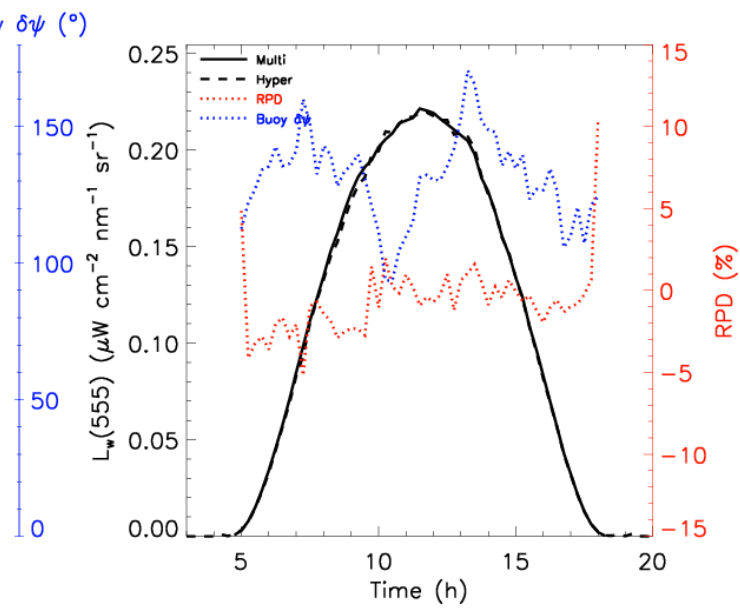
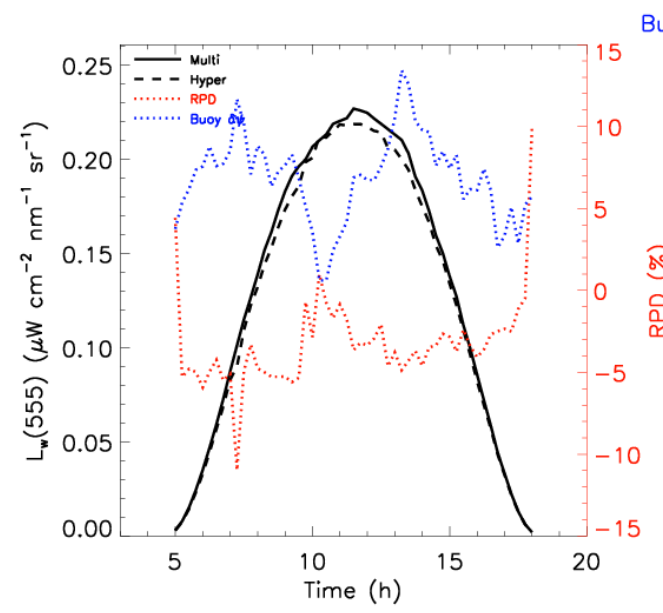
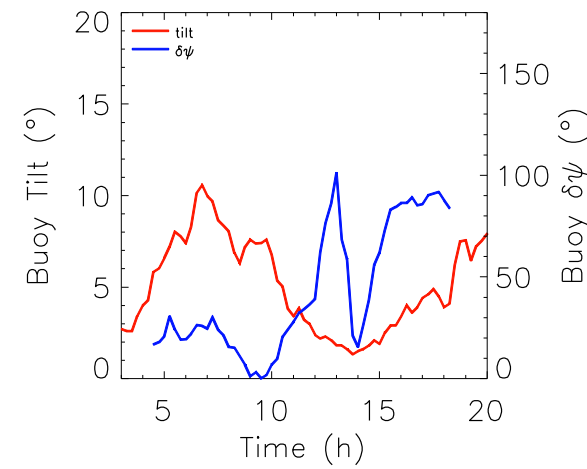
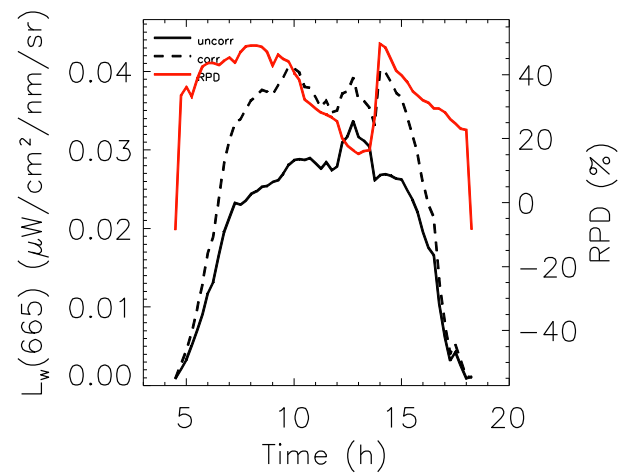
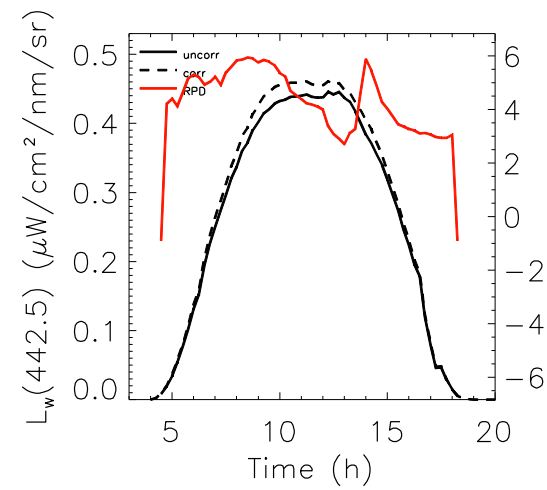
- > Backward 3D *Montecarlo* simulation (*Simulo*) replaces the *Gordon & Ding (1992)* correction scheme
- > Simulation for each underwater instrument
 - Chl = 0.1, 0.5, 1.0, 5.0 $\mu\text{g l}^{-1}$
 - Azimuth angle from 0° to 360° , with 5° step
 - Zenith angle from 0° to 90° , with 5° step
 - 7 wavelengths (412, 443, 490, 510, 555, 670 nm)
- > A correction factor from LUTs is applied
 - $L_u(z_4, t, \lambda) = L_u(z_4, t, \lambda)' \cdot f_{S4}$
 - $L_u(z_9, t, \lambda) = L_u(z_9, t, \lambda)' \cdot f_{S9}$



_BoueFullLu4m_443_0.1 N= 6.0e+09

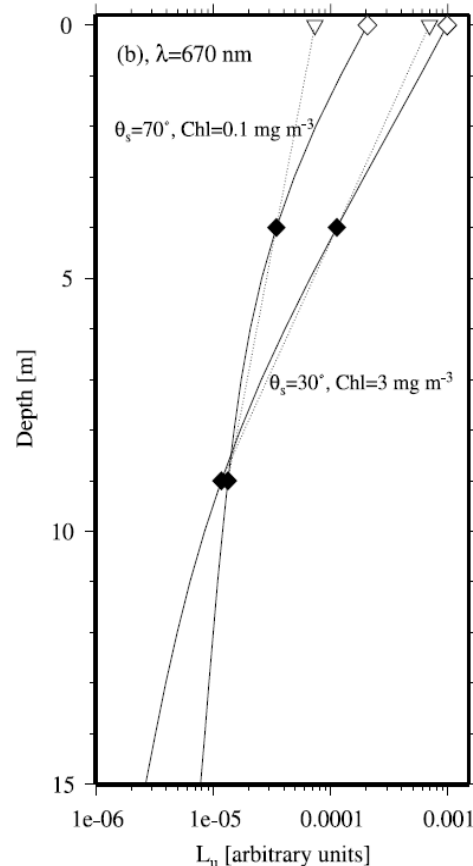
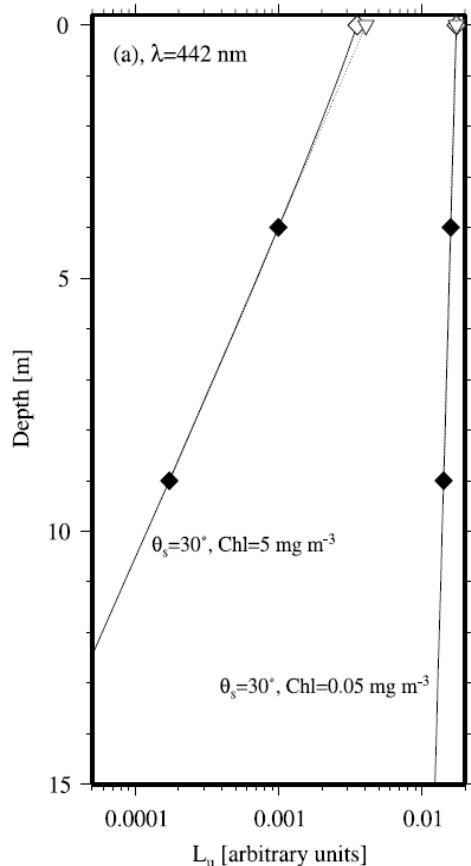
Shade Average 30–60 deg





EXTRAPOLATION OF L_u TO SURFACE

- > Diffuse attenuation coefficient for radiance is estimated from the L_u measurements at 4 m and 9 m
 - $$K_L = -\frac{\ln[L_u(z_9, t, \lambda) / L_u(z_4, t, \lambda)]}{z_9 - z_4}$$
- > L_u at 4 m is then lognormally extrapolated to surface (below water) and a correction factor is applied*
 - $$L_u(0^-, t, \lambda) = \overline{L_u(z_4, t, \lambda)} e^{-z_4 \cdot K_L} \cdot f_H$$
- > Finally water leaving radiance is calculated as
 - $$L_w(t, \lambda) = L_u(0^-, t, \lambda) \cdot \frac{1-\rho}{n^2} ; \text{ where } \frac{1-\rho}{n^2} = 0.543$$



*HYDROLIGHT CORRECTION

- > Radiative transfer simulation of $L_u(z, \text{Chl}, \theta_s, \lambda)$
 - Chl = 0.1, 0.5, 1.0, 5.0 $\mu\text{g l}^{-1}$
 - Zenith angle from 0° to 90° , with 5° step
 - 7 wavelengths (412, 443, 490, 510, 555, 670 nm)
- > Generation of a LUT of the ratio between $L_u(0^-, t, \lambda)$ as estimated from radiative transfer simulations and lognormal extrapolation of simulated $L_u(\text{Chl}, \theta_s, \lambda)$ at 4 and 9 m

$$R_{rs}(t, \lambda) = \frac{L_w(t, \lambda)}{E_s(t, \lambda)}$$



$$R_{rs} = \frac{\overline{L_{u4}} f_{cal} f_{s4} \exp \left[z_4 \left(\frac{-\ln(\overline{L_{u9}} f_{cal} f_{s9} / \overline{L_{u4}} f_{cal} f_{s4})}{z_9 - z_4} \right) \right] f_H f_{\rho n}}{\overline{E_s} f_{cal} f_{cos} f_{tilt} f_{dir} + (1 - f_{dir}) \overline{E_s} f_{cal}}$$

KEEP IN MIND FOR THE NEXT TALK

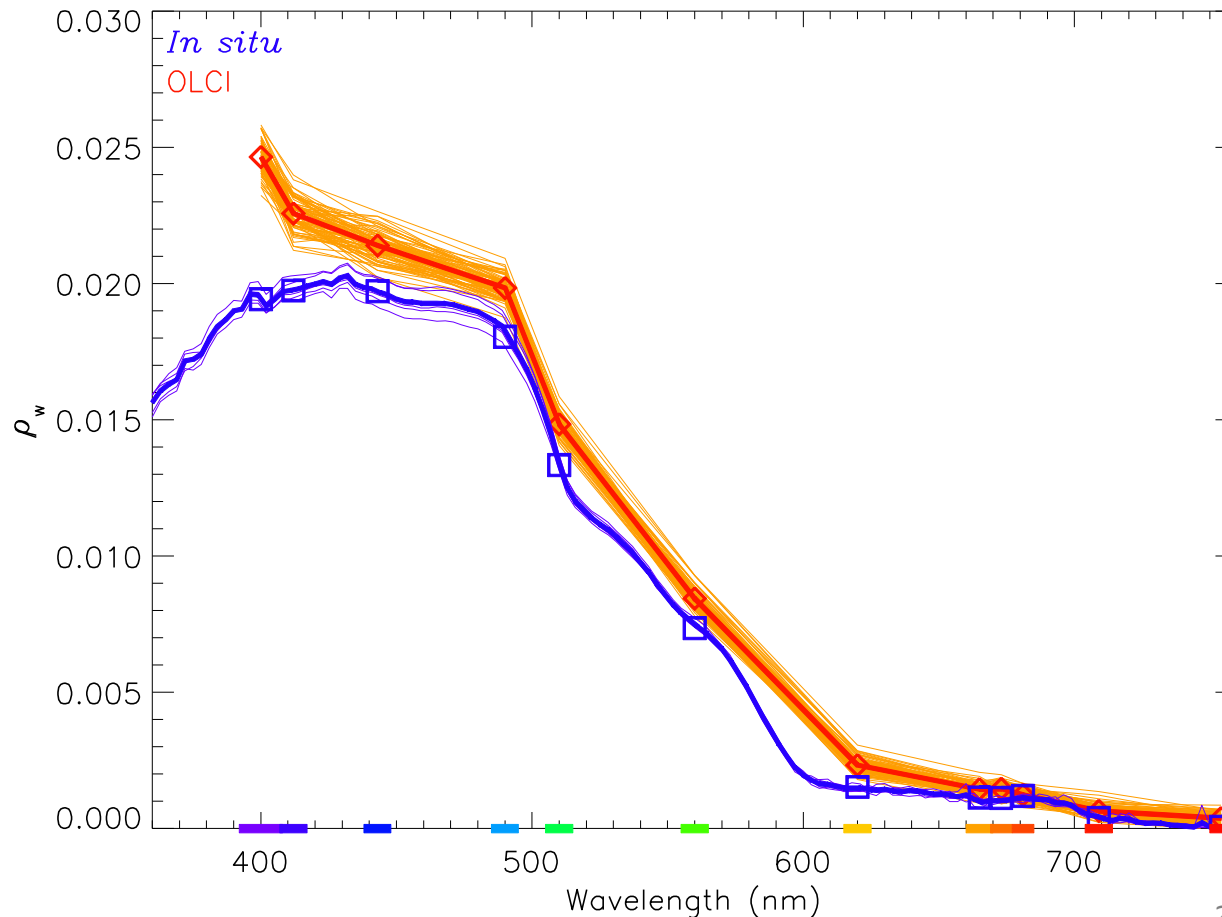
- $\overline{E_s} = \overline{E_s(t, \lambda)'} \left. \vphantom{\overline{E_s}} \right\}$
- $\overline{L_{u4}} = \overline{L_u(4, t, \lambda)'} \left. \vphantom{\overline{L_{u4}}} \right\}$ Median of 1' records corrected for dark drift
- $\overline{L_{u9}} = \overline{L_u(9, t, \lambda)'} \left. \vphantom{\overline{L_{u9}}} \right\}$
- $f_{cal} = 1$ next talk for more details

- > Product delivered to space agencies, from here data processing for match-up analysis might differ

HYPERSPECTRAL INSTRUMENTS

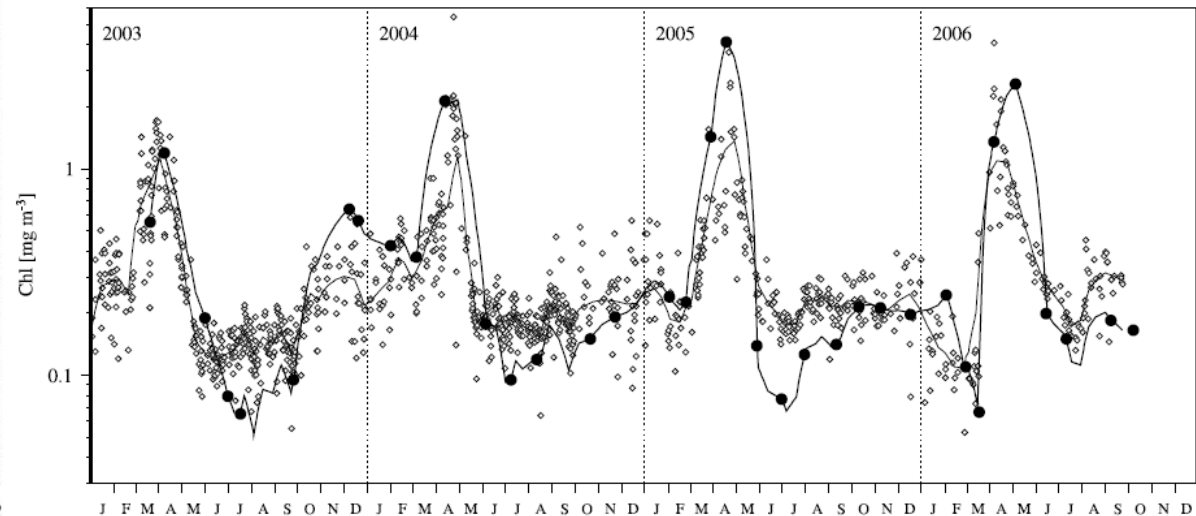
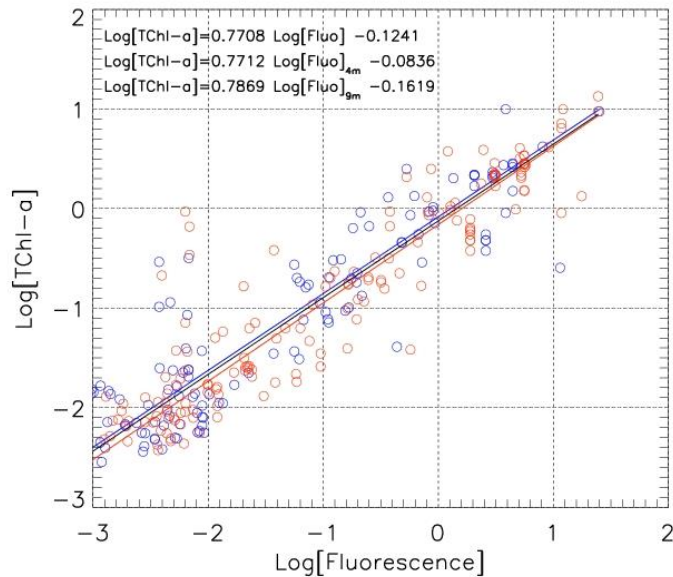
$$- R_{rs}(t, \lambda_i)_{sat} = \frac{\int_{\lambda_{i,0}}^{\lambda_{i,n}} L_w(t, \lambda_i) \cdot SRF(\lambda_i)_{sat} d\lambda}{\int_{\lambda_{i,0}}^{\lambda_{i,n}} SRF(\lambda_i)_{sat} d\lambda} \cdot \frac{\int_{\lambda_{i,0}}^{\lambda_{i,n}} E_s(t, \lambda_i) \cdot SRF(\lambda_i)_{sat} d\lambda}{\int_{\lambda_{i,0}}^{\lambda_{i,n}} SRF(\lambda_i)_{sat} d\lambda}$$

$SRF(\lambda_i)_{sat}$ are the spectral response functions of SeaWiFS, MERIS, MODIS, VIIRS, MSI, OLCI



TCHL-A TIME SERIES

- > TChl-a values are needed for LUTs of shading and *HydroLight* corrections (a single value per day is used)
- > For recent data TChl-a values comes from calibrated Fluorescence calibrated (linear regression of an historical data set VS HPLC, mean night value are used to eliminate data affected by non-photochemical quenching)
- > For assessed data a time-series from satellite data calibrated on monthly HPLC is used.



SOME CRITERIA GENERALLY USED FOR QC

- > Buoy depths < 11 m are discarded (E_s too close to sea surface)
- > Buoy Tilt > 10°
- > $0.8 < E_s/\text{Theoretical } E_s < 1.2$

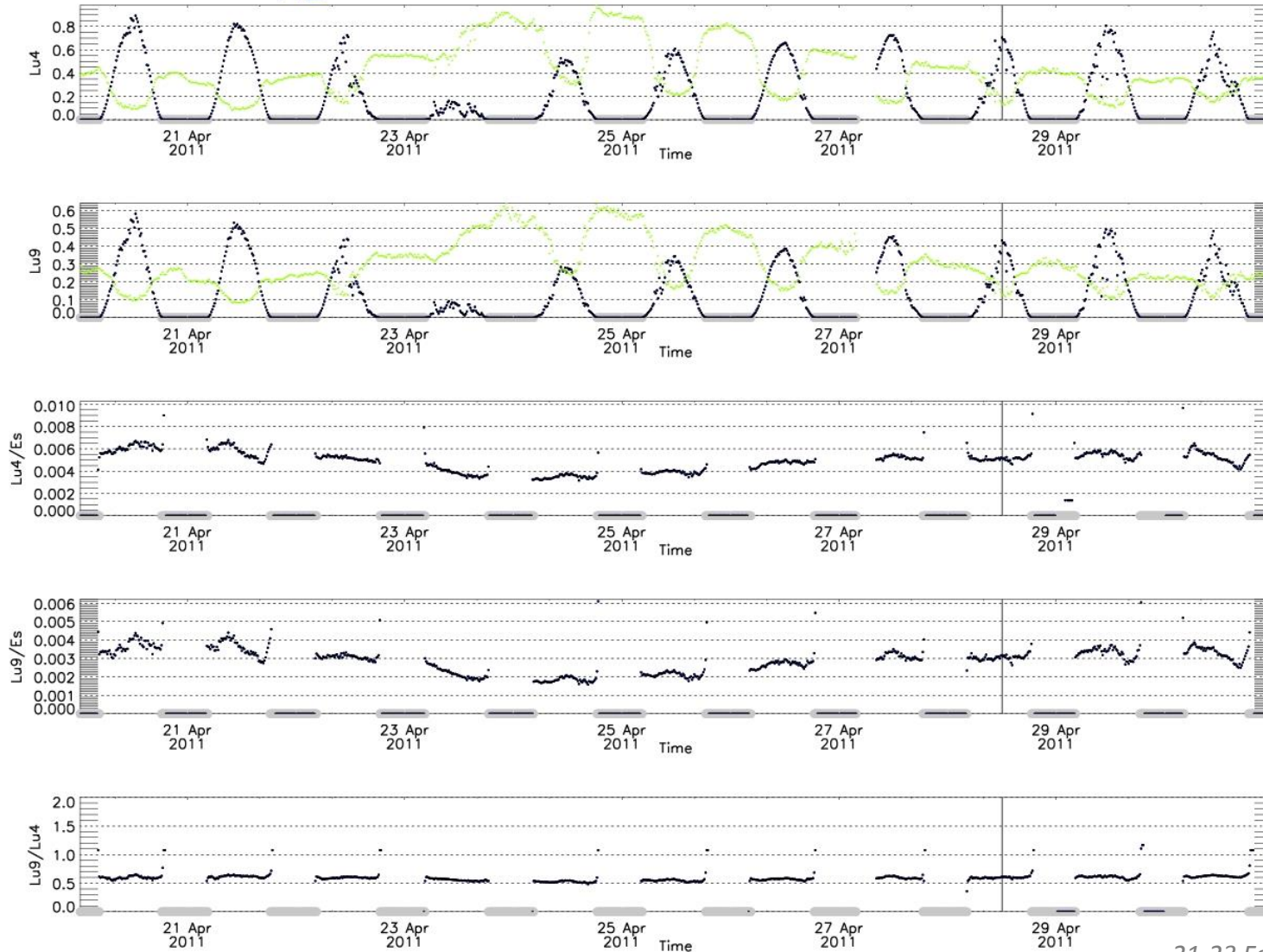
FINER CRITERIA NOT ROUTINELY USED

- > Standard deviation of E_s < 2%
- > Azimuth angle (i.e. shading correction)
- > Further QC is performed case per case on specific data sets

BIOFOULING

- > Data screening for possible presence of biofouling (sensor cleaning helps)
- > Elimination or correction whenever possible

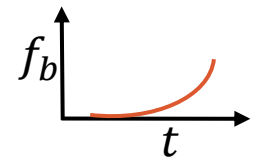
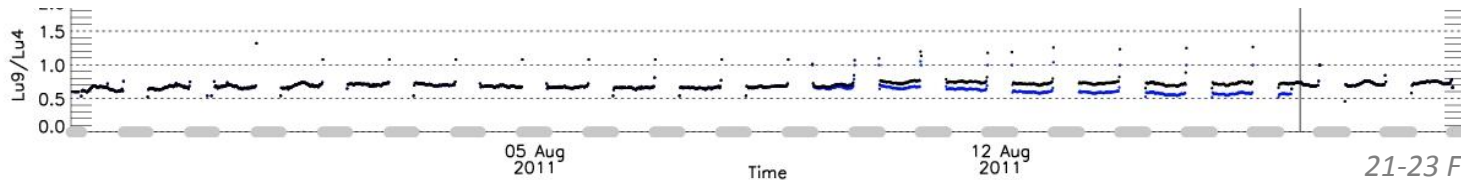
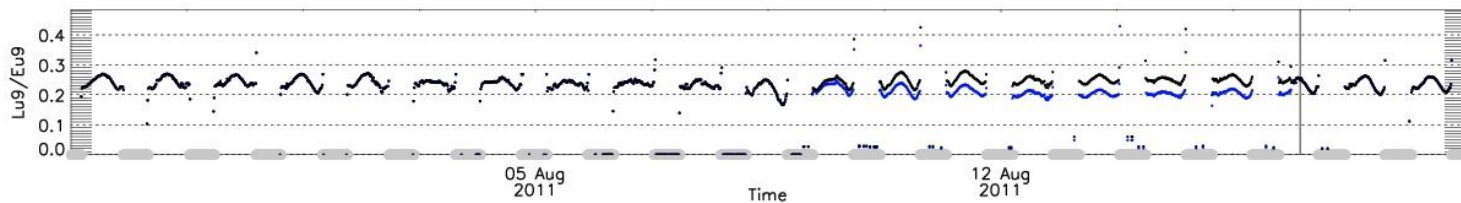
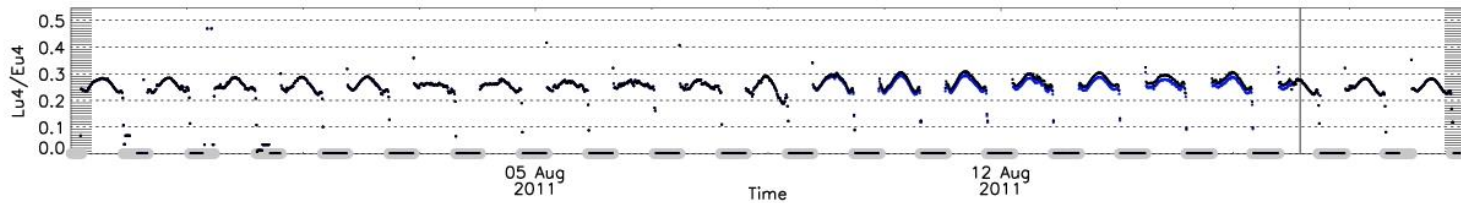
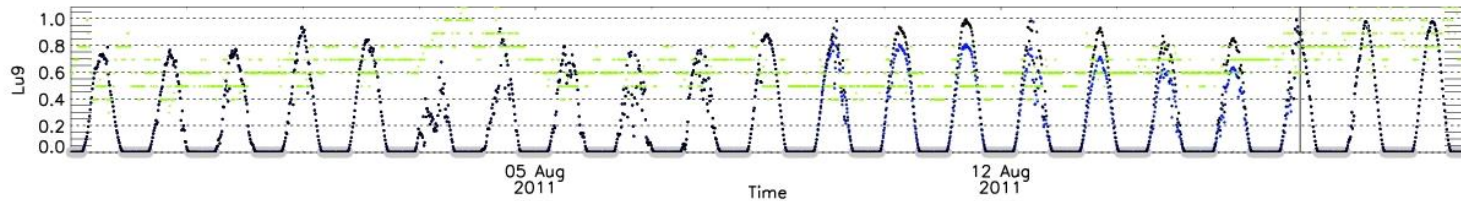
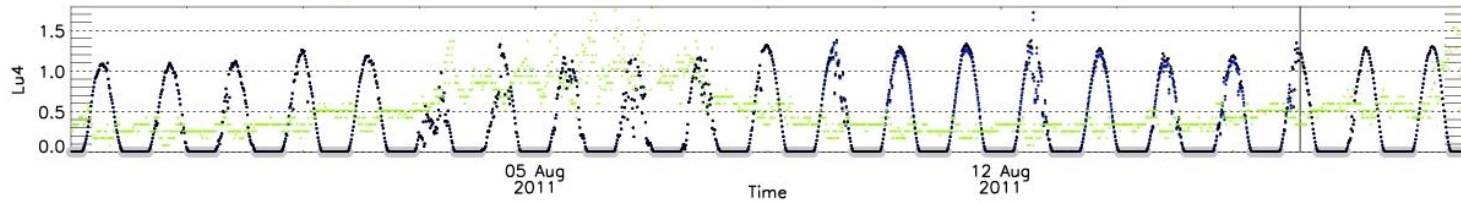
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BIOFOULING

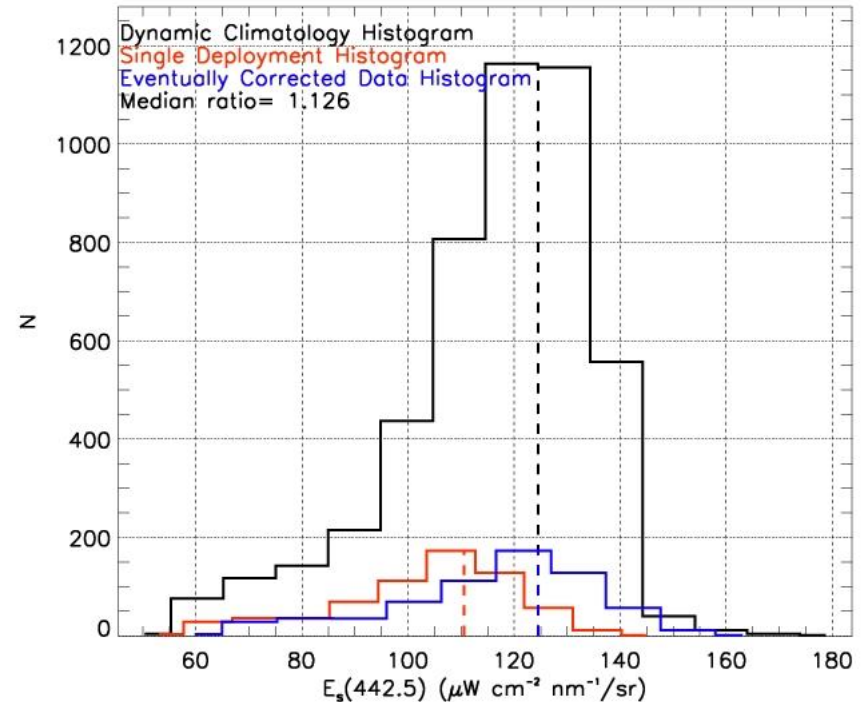
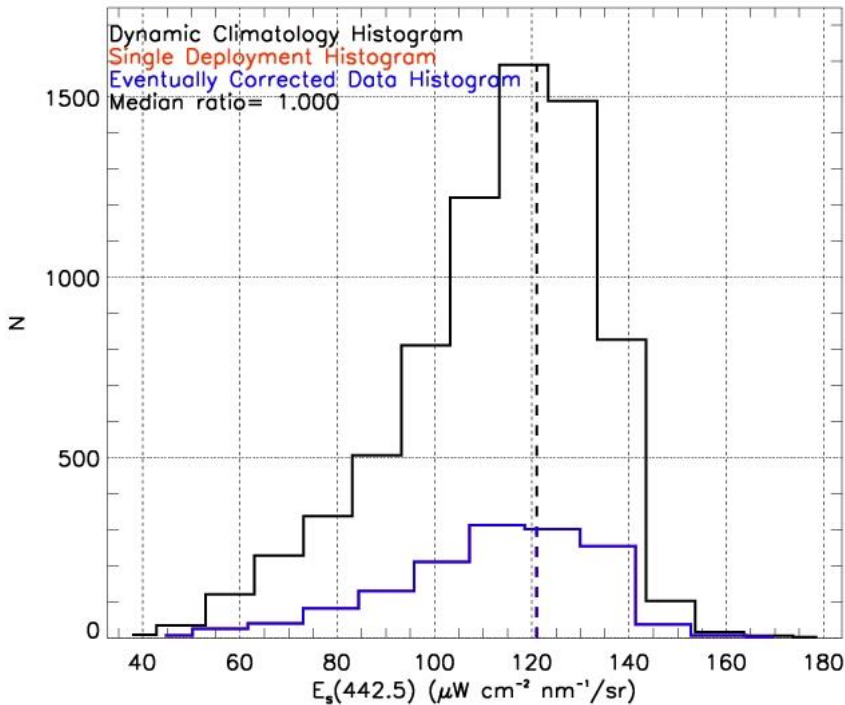
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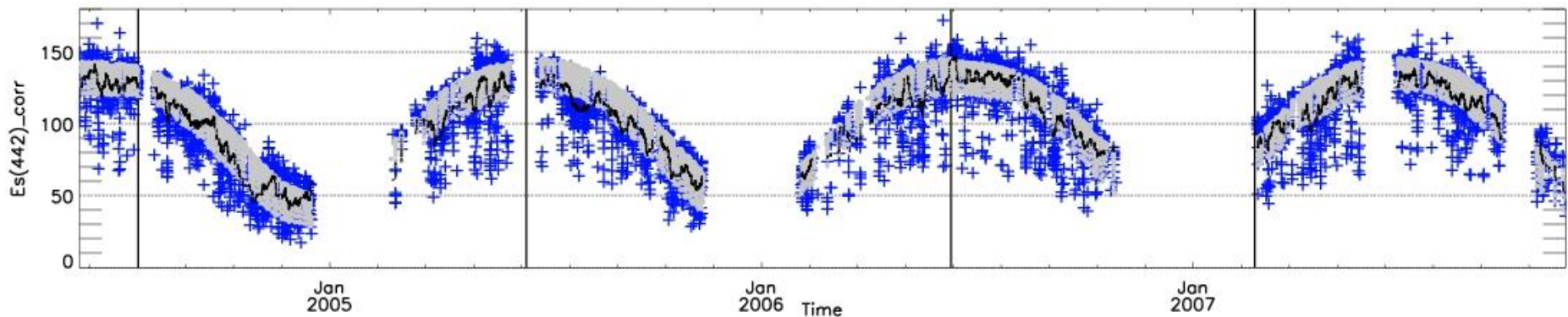
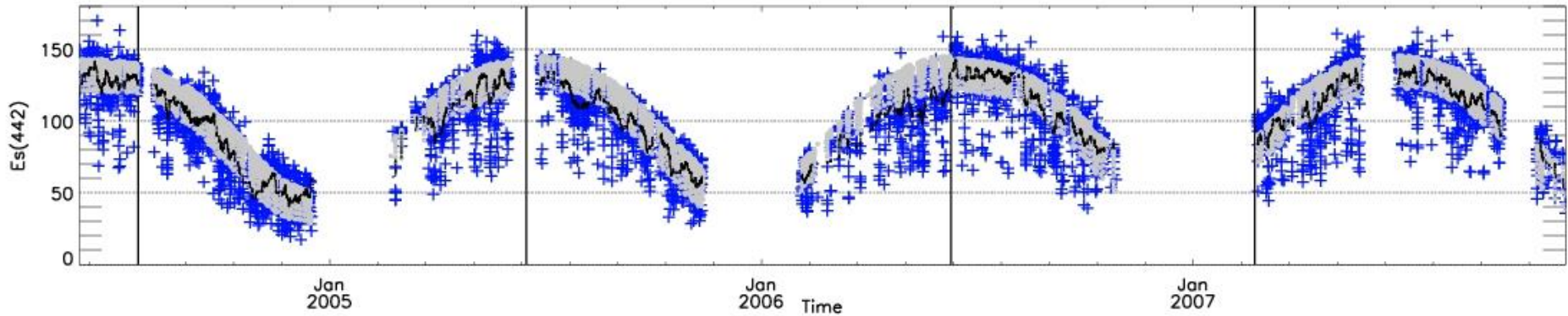
DYNAMIC CLIMATOLOGY CORRECTION

- > Data from deployments (or partial deployments from known issues) are compared to the rest of data from the same period of the year in terms of median ratio
- > Data whose median ratio is within a threshold are retained in the "good" data set
- > Thresholds are $\text{Log}(\text{median ratio}) < |0.1|$ for E_s , $\text{Log}(\text{median ratio}) < |0.2|$ for Lu , Ed , Eu
- > A "good" data set is established for each wavelength, instrument, depth
- > "Bad data" are compared to its corresponding "good" dynamic climatology and a correction factor estimated
- > Keep in mind that in most cases 1/few wavelengths of one of three instruments used to derive Rrs are concerned



DYNAMIC CLIMATOLOGY CORRECTION

- > How does it look like in a time series?
- > The procedure still need to be settled (*i.e.*: definition of the thresholds and N of observations needed in the dynamic climatology to asses stable "gains")



PURPOSE OF THESE CORRECTIONS

- > Biofouling and Intercalibration corrections are not intended for SVC use
- > Still valuable data for science (eg: seasonal variability, modelling assimilation,...)
- > Debatable use for validation : the definitive answer can be given after assessment of their uncertainties (to do list)

THANKS FOR ATTENTION

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M. Golbol, E. Soto, E. Diamond – Cruises
V. Taillander – CTD processing
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B. Gentili – Code development
A. Bialek – Uncertainties
E. Leymarie – Montecarlo simulations
Bricaud – CDOM
G. De Liege, D. Luquet, D. Robin – Diving
S. Marty – Calibrations
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L. Fere, C. Poutier, I. Courtois – Administration

